

Chapter 3. The Importance of State Functions. The Internal Energy and Enthalpy

Summary

- useful features of state functions are identified
- introduction to the mathematics of thermodynamic partial differential equations
- changes in the internal energy and enthalpy are related to easily measured changes in the state variables T , V , and p
- applications: * Joule-Thomson experiment
* liquefaction of gases

Section 3.1 Mathematical Properties of State Functions: Partial Differential Equations

Partial Differential equations - the “language” of thermodynamics
(and many other branches of science and technology)

- What are **differential equations**?
- What are “**partial**” differential equations?
- Why are differential equations important?
- How can they be used?
- What rules apply?

First ... **“Ordinary” Differential Equations**

only one independent variable

Example: independent variable x in the function $f(x) = 10x^3 - 3x$

derivative of $f(x)$

[slope of $f(x)$ plotted against x]

$$\frac{df(x)}{dx} = \lim_{\Delta x \rightarrow 0} \frac{f(x + \Delta x) - f(x)}{\Delta x}$$

integral of $f(x)$

“add up” the df differentials

[gives the change in $f(x)$]

$$\Delta f = f(x_b) - f(x_a) = \int_{x_a}^{x_b} \frac{df(x)}{dx} dx = \int_{f(x_a)}^{f(x_b)} df$$

But thermodynamic functions generally depend on two or more independent variables

Example

The pressure of n moles of ideal gas is a function of T and V .

$$p(T, V) = \frac{nRT}{V}$$

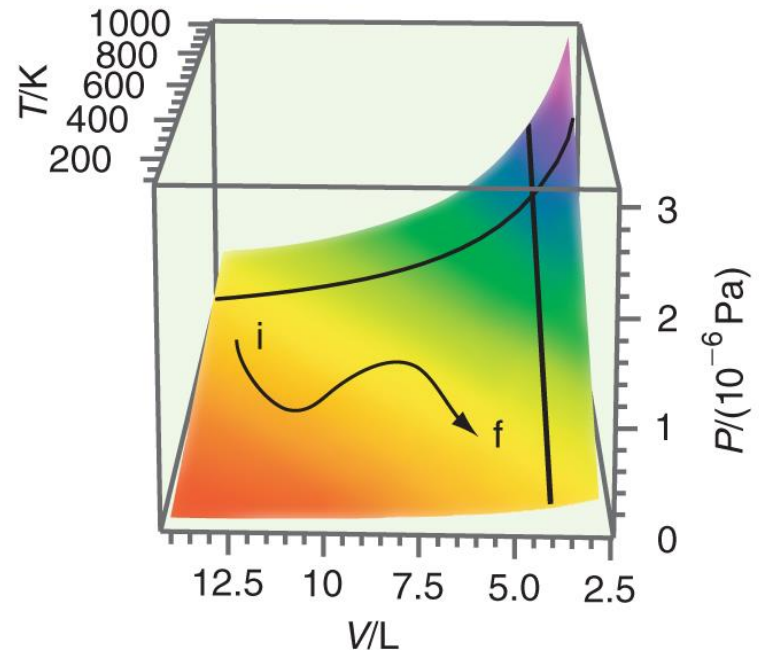
Ordinary derivatives

$$\frac{dp}{dT} \quad ? \quad \frac{dp}{dV} \quad ?$$

are ambiguous and do not apply.

Why? At each point $p(T, V)$ an infinite number of different slopes dp/dT and dp/dV exist in an infinite number of different directions.

$p(T, V)$ surface



“Partial” Derivatives *to the Rescue*

For the derivatives of the function $p(T, V)$, to avoid ambiguity, define the partial derivatives:

$$\left(\frac{\partial p}{\partial T} \right)_V = \lim_{\Delta T \rightarrow 0} \frac{p(T + \Delta T, V) - p(T, V)}{\Delta T}$$

slope of p against T
parallel to the T axis
(V fixed)

(Why “partial”? Only T and p are changing.)

$$\left(\frac{\partial p}{\partial V} \right)_T = \lim_{\Delta V \rightarrow 0} \frac{p(T, V + \Delta V) - p(T, V)}{\Delta V}$$

slope of p against V
parallel to the V axis
(T fixed)

(Only V and p are changing.)

Other Partial Differential Equations

1. Wave Equation

Vibration of an elastic string in one dimension:

$$\frac{\partial^2 u}{\partial t^2} = c^2 \frac{\partial^2 u}{\partial x^2}$$

$u(x,t)$ is the displacement at time t and position x along the string.
 c is the speed of the vibration moving along the string.

Three-dimensional vibration of an elastic medium (such as sound waves, ultrasonic or seismic waves):

$$\frac{\partial^2 u}{\partial t^2} = c^2 \frac{\partial^2 u}{\partial x^2} + c^2 \frac{\partial^2 u}{\partial y^2} + c^2 \frac{\partial^2 u}{\partial z^2} = c^2 \nabla^2 u$$

2. Heat Conduction Equation

Heat conduction in one dimension:

$$\frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial x^2}$$

$T(x,t)$ is the temperature at time t and position x .

k is the thermal conductivity.

Three-dimensional heat conduction:

$$\frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial x^2} + k \frac{\partial^2 T}{\partial y^2} + k \frac{\partial^2 T}{\partial z^2} = k \nabla^2 T$$

3. Diffusion Equation

Diffusion in one dimension:

$$\frac{\partial C_A}{\partial t} = D \frac{\partial^2 C_A}{\partial x^2}$$

$C_A(x,t)$ is the concentration of chemical A at time t and position x .
 D is the diffusion coefficient.

Three-dimensional diffusion:

$$\frac{\partial C_A}{\partial t} = D \frac{\partial^2 C_A}{\partial x^2} + D \frac{\partial^2 C_A}{\partial y^2} + D \frac{\partial^2 C_A}{\partial z^2} = D \nabla^2 C_A$$

4. Equation of Continuity for Fluid Flow

Fluid flow in one dimension:

$$\frac{\partial \rho}{\partial t} = - \frac{\partial (\rho v_x)}{\partial x}$$

$\rho(x,t)$ is the density of the fluid at time t and position x .
 v_x is the velocity of the fluid in the x direction.

Three-dimensional continuity equation:

$$\frac{\partial \rho}{\partial t} = - \frac{\partial (\rho v_x)}{\partial x} - \frac{\partial (\rho v_y)}{\partial y} - \frac{\partial (\rho v_z)}{\partial z}$$

5. Transmission Line Equation

Flow of electric current $I(x,t)$ along a wire:

$$\frac{\partial^2 I}{\partial x^2} = LC \frac{\partial^2 I}{\partial t^2} + (RC + GL) \frac{\partial I}{\partial t} + RGI$$

x is the position along the wire

R is the resistance

C is the capacitance

L is the induction

G is the loss

6. Lagrangian Equations of Motion

L = kinetic energy – potential energy for a mechanical system

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_i} \right) = \frac{\partial L}{\partial q_i}$$

q_i is the generalized position of mass i (*any* coordinate system)

\dot{q}_i is the generalized velocity of mass i

7. Schrodinger Quantum Mechanical Equation

$$-\frac{h^2}{8\pi^2m} \left(\frac{\partial^2\psi}{\partial x^2} + \frac{\partial^2\psi}{\partial y^2} + \frac{\partial^2\psi}{\partial z^2} \right) + V\psi = E\psi$$

h = Planck constant

V = potential energy

E = total energy

m = particle mass

ψ = wave function

Solving the Schrodinger equation for an electron in the electric potential energy field of a proton gives the ψ_{1s} , ψ_{2s} , ψ_{2p} , ψ_{3s} , ... orbitals used by chemists

Example: Partial Derivatives of $p(T,V)$ for an Ideal Gas

partial T derivative:

$$\left(\frac{\partial p}{\partial T}\right)_V = \left(\frac{\partial[nRT/V]}{\partial T}\right)_V = \frac{nR}{V} \left(\frac{\partial T}{\partial T}\right)_V$$

n, R, V constant

$$= \frac{nR}{V} = \frac{p}{T}$$

1

partial V derivative:

$$\left(\frac{\partial p}{\partial V}\right)_T = \left(\frac{\partial[nRT/V]}{\partial V}\right)_T = nRT \left(\frac{\partial \frac{1}{V}}{\partial V}\right)_T = nRT \left(\frac{-1}{V^2}\right)$$

n, R, T constant

same as $d(1/V) / dV$ at fixed T

$$= -\frac{nRT}{V^2} = -\frac{p}{V}$$

“Exact” Differential of $p(T,V)$

Because p is a function of state variables T and V :

- a) the infinitesimal change in p (the differential dp) produced by changes dT and dV is **exactly defined** (not path-dependent):

$$dp = \left(\frac{\partial p}{\partial T} \right)_V dT + \left(\frac{\partial p}{\partial V} \right)_T dV$$

- b) the change in p obtained by integrating dp is **exactly defined** by the initial state $p_i(T_i, V_i)$ and the final state $p_f(T_f, V_f)$ (also not path-dependent)

$$\Delta p = \int_{T_i, V_i}^{T_f, V_f} dp = p_f(T_f, V_f) - p_i(T_i, V_i)$$

Useful Rules for Partial Derivatives

Inverse Rule

$$\left(\frac{\partial p}{\partial T}\right)_V = \frac{1}{\left(\frac{\partial T}{\partial p}\right)_V}$$

Cyclic Rule

(why cyclic?)

$$\left(\frac{\partial p}{\partial T}\right)_V \left(\frac{\partial T}{\partial V}\right)_p \left(\frac{\partial V}{\partial p}\right)_T = -1$$

Using the inverse rule, the cyclic rule is also written as:

*Buy two partial derivatives,
get one free!*

$$\left(\frac{\partial p}{\partial T}\right)_V = -\left(\frac{\partial p}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_p$$

Where Does the Cyclic Rule Come From?

$$dp = \left(\frac{\partial p}{\partial T} \right)_V dT + \left(\frac{\partial p}{\partial V} \right)_T dV$$

divide by dT at constant p
($dp = 0$)

$$0 = \left(\frac{\partial p}{\partial T} \right)_V \frac{dT}{dT_p} + \left(\frac{\partial p}{\partial V} \right)_T \frac{dV}{dT_p}$$

$$0 = \left(\frac{\partial p}{\partial T} \right)_V (1) + \left(\frac{\partial p}{\partial V} \right)_T \left(\frac{\partial V}{\partial T} \right)_p$$

$$\left(\frac{\partial p}{\partial T} \right)_V = - \left(\frac{\partial p}{\partial V} \right)_T \left(\frac{\partial V}{\partial T} \right)_p$$

Cyclic Rule

*Why the minus sign
in the Cyclic Rule?*

At constant p , the change in p caused by dT cancels the change in p caused by dV so that $dp = 0$.

notice: $\left(\frac{\partial p}{\partial T} \right)_V \neq \left(\frac{\partial p}{\partial V} \right)_T \left(\frac{\partial V}{\partial T} \right)_p$

Why? dV at constant T does not equal dV at constant p .

Mixed Partial Derivatives: Order of Differentiation of a Function Doesn't Matter

∂T first, then ∂V

∂V first, then ∂T

Example:
$$\left[\frac{\partial}{\partial V} \left(\frac{\partial p}{\partial T} \right)_V \right]_T = \left[\frac{\partial}{\partial T} \left(\frac{\partial p}{\partial V} \right)_T \right]_V$$

Can be used as a test to show $dp = \left(\frac{\partial p}{\partial T} \right)_V dT + \left(\frac{\partial p}{\partial V} \right)_T dV$ is an exact differential.

Exercise For an ideal gas ($p = nRT/V$), verify:

$$\left[\frac{\partial}{\partial V} \left(\frac{\partial p}{\partial T} \right)_V \right]_T = -\frac{nR}{V^2} = \left[\frac{\partial}{\partial T} \left(\frac{\partial p}{\partial V} \right)_T \right]_V$$

Proof (a bit tricky)

$$\begin{aligned} \left[\frac{\partial}{\partial T} \left(\frac{\partial p}{\partial V} \right)_T \right]_V &= \left[\frac{\partial}{\partial T} \left(\lim_{\Delta V \rightarrow 0} \frac{p(T, V + \Delta V) - p(T, V)}{\Delta V} \right) \right]_V \\ &= \lim_{\Delta T \rightarrow 0} \left(\lim_{\Delta V \rightarrow 0} \frac{\frac{p(T + \Delta T, V + \Delta V) - p(T + \Delta T, V)}{\Delta V} - \frac{p(T, V + \Delta V) - p(T, V)}{\Delta V}}{\Delta T} \right) \\ &= \lim_{\Delta V \rightarrow 0} \left(\lim_{\Delta T \rightarrow 0} \frac{\frac{p(T + \Delta T, V + \Delta V) - p(T, V + \Delta V)}{\Delta T} - \frac{p(T + \Delta T, V) - p(T, V)}{\Delta T}}{\Delta V} \right) \\ &= \left[\frac{\partial}{\partial V} \left(\lim_{\Delta T \rightarrow 0} \frac{p(T + \Delta T, V) - p(T, V)}{\Delta T} \right) \right]_T \\ &= \left[\frac{\partial}{\partial V} \left(\frac{\partial p}{\partial T} \right)_V \right]_T \end{aligned}$$

Important Application: p - V - T Calculations

Useful and convenient (intensive) experimental quantities:

Volumetric Thermal Expansion Coefficient β

$$\beta = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_p$$

gives the **fractional** change in volume per Kelvin

β is usually (but not always) positive.

Isothermal Compressibility κ (also called κ_T)

$$\kappa = -\frac{1}{V} \left(\frac{\partial V}{\partial p} \right)_T$$

gives the negative **fractional** change in volume per Pa

$(\partial V/\partial p)_T$ is always negative, so κ is always positive.

TABLE 3.1 Volumetric Thermal Expansion Coefficient for Solids and Liquids at 298 K

Element	$10^6 \beta / (\text{K}^{-1})$	Element or Compound	$10^4 \beta / (\text{K}^{-1})$
Ag(<i>s</i>)	57.6	Hg(<i>l</i>)	1.81
Al(<i>s</i>)	69.3	CCl ₄ (<i>l</i>)	11.4
Au(<i>s</i>)	42.6	CH ₃ COCH ₃ (<i>l</i>)	14.6
Cu(<i>s</i>)	49.5	CH ₃ OH(<i>l</i>)	14.9
Fe(<i>s</i>)	36.9	C ₂ H ₅ OH(<i>l</i>)	11.2
Mg(<i>s</i>)	78.3	C ₆ H ₅ CH ₃ (<i>l</i>)	10.5
Si(<i>s</i>)	7.5	C ₆ H ₆ (<i>l</i>)	11.4
W(<i>s</i>)	13.8	H ₂ O(<i>l</i>)	2.04
Zn(<i>s</i>)	90.6	H ₂ O(<i>s</i>)	1.66

Sources: Benenson, W., Harris, J. W., Stocker, H., and Lutz, H. *Handbook of Physics*. New York: Springer, 2002; Lide, D. R., ed. *Handbook of Chemistry and Physics*. 83rd ed. Boca Raton, FL: CRC Press, 2002; Blachnik, R., ed. *D'Ans Lax Taschenbuch für Chemiker und Physiker*. 4th ed. Berlin: Springer, 1998.

Note: for H₂O(liquid) at 0 °C, $\beta = -5.47 \times 10^{-5} \text{ K}^{-1}$ (shrinks when heated!)

Application of thermal expansion ...

Liquid-in-Glass Thermometers

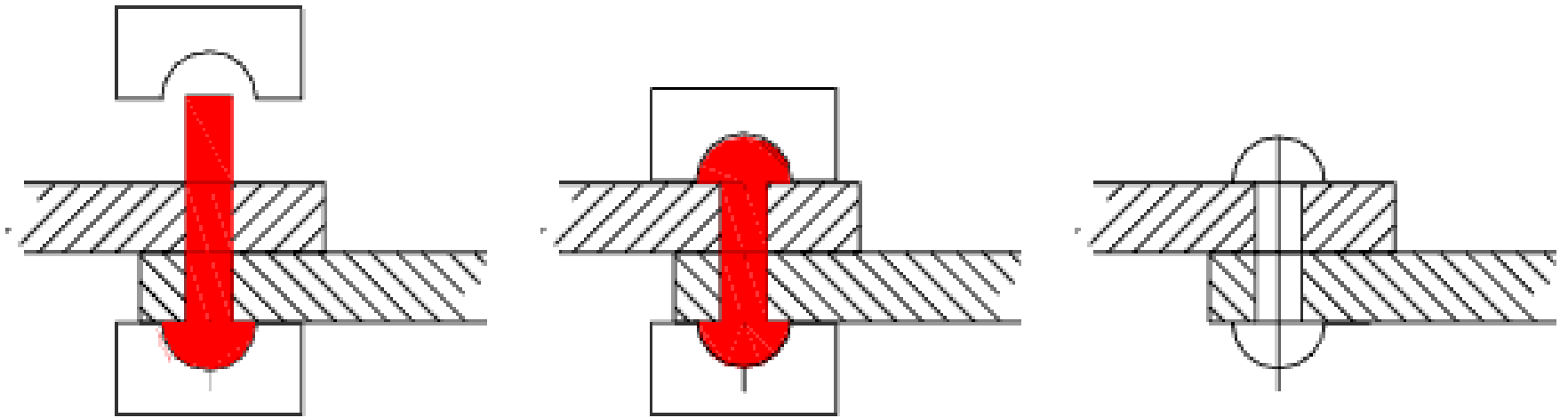
Liquid when heated expands more than the glass.

$$\beta_{\text{liquid}} > \beta_{\text{glass}}$$

Related: *Why can warm water sometimes be used to get a tight lid off a glass jar?*

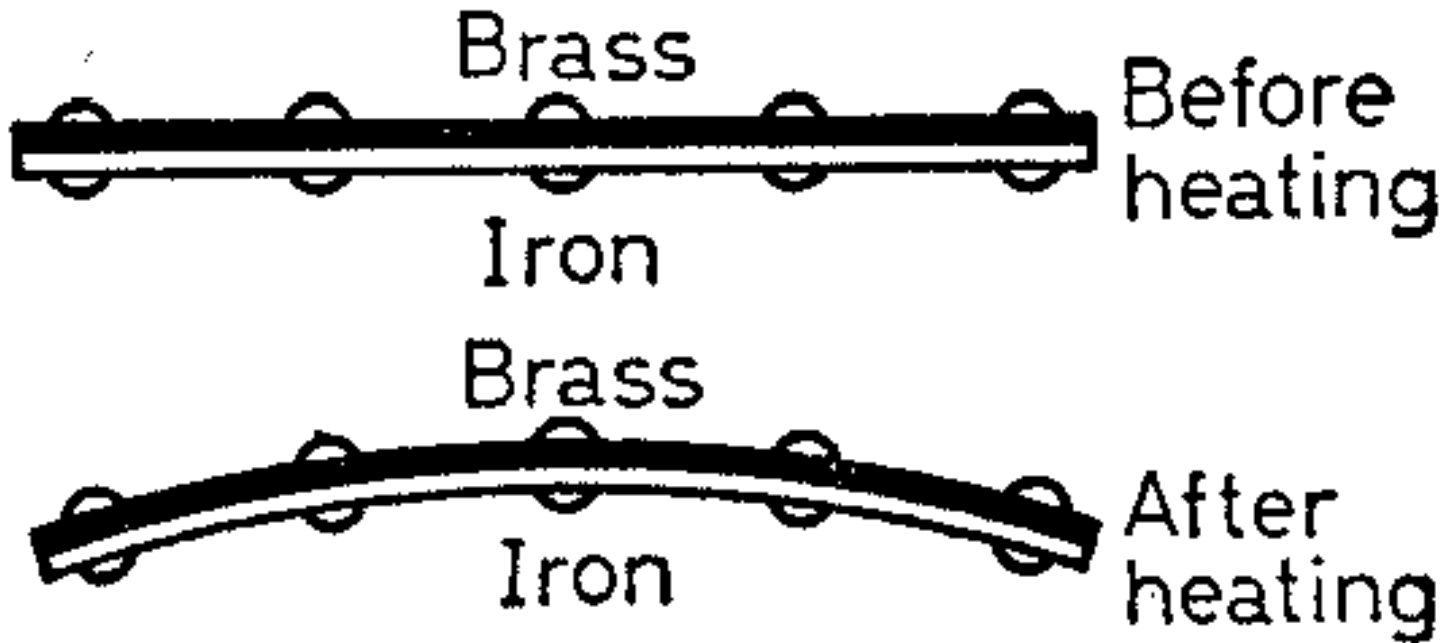


Hot Rivet Fasteners



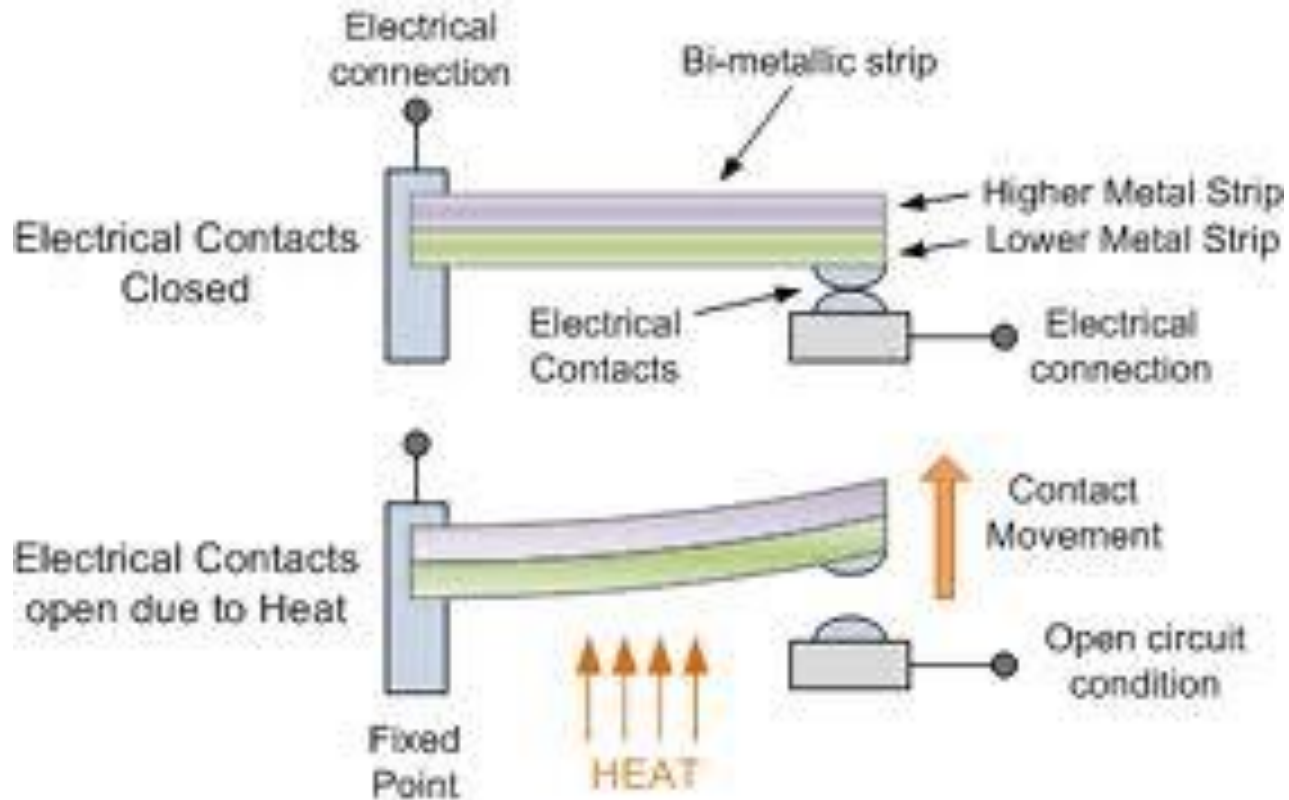
Hot rivet shrinks as it cools, tightly fastening two metal pieces.

Bimetallic Strip



$$\beta_{\text{Brass}} > \beta_{\text{Iron}}$$

Bimetallic Strip



thermostat switch to turn off the furnace

Volumetric Thermal Expansion Coefficient β

$$\beta = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_p \quad \text{fractional change in volume per degree}$$

Linear Thermal Expansion Coefficient β_{linear}

$$\beta_{\text{linear}} = \frac{1}{\ell} \left(\frac{\partial \ell}{\partial T} \right)_p = \frac{1}{3} \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_p = \frac{\beta}{3} \quad \text{Can you show this?}$$

fractional change in length per degree

Example

If the average temperature of the oceans increases by 1 °C, what is the increase in sea level?

Data: The average volumetric thermal expansion coefficient of seawater is $\beta = 0.00011 \text{ K}^{-1}$. The average depth of the oceans is 3.7 km.

$$\text{From } \beta_{\text{linear}} = \frac{1}{\ell} \left(\frac{\partial \ell}{\partial T} \right)_p \quad \text{get} \quad \beta_{\text{linear}} dT = \frac{d\ell}{\ell} = \frac{\beta}{3} dT$$

$$\beta_{\text{linear}} \int_T^{T+\Delta T} dT = \int_{\ell(T)}^{\ell(T+\Delta T)} \frac{d\ell}{\ell} \quad \beta_{\text{linear}} (\Delta T) = \ln \left(\frac{\ell(T+\Delta T)}{\ell(T)} \right)$$

$$\frac{\ell(T+\Delta T)}{\ell(T)} = \exp[\beta_{\text{linear}} (\Delta T)] = \exp \left[\frac{0.00011 \text{ K}^{-1}}{3} 1 \text{ K} \right] = 1.000037$$

$$0.0037 \% \text{ of } 3.7 \text{ km} = 0.000037 \times 3.7 \text{ km} = 0.00014 \text{ km} = \mathbf{0.14 \text{ m}}$$

What's this? What does it have to do with thermal expansion?



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Concorde Supersonic (Mach 2.0) Passenger Aircraft



At cruising speed, twice the speed of sound, air friction heated the skin to about 150 °C, increasing the length of the aircraft by about one foot, an important design consideration for maintaining structural integrity.

TABLE 3.2 Isothermal Compressibility at 298 K

Substance	$10^6 \kappa/\text{bar}^{-1}$	Substance	$10^6 \kappa/\text{bar}^{-1}$
Al(<i>s</i>)	1.33	Br ₂ (<i>l</i>)	64
SiO ₂ (<i>s</i>)	2.57	C ₂ H ₅ OH(<i>l</i>)	110
Ni(<i>s</i>)	0.513	C ₆ H ₅ OH(<i>l</i>)	61
TiO ₂ (<i>s</i>)	0.56	C ₆ H ₆ (<i>l</i>)	94
Na(<i>s</i>)	13.4	CCl ₄ (<i>l</i>)	103
Cu(<i>s</i>)	0.702	CH ₃ COCH ₃ (<i>l</i>)	125
C(graphite)	0.156	CH ₃ OH(<i>l</i>)	120
Mn(<i>s</i>)	0.716	CS ₂ (<i>l</i>)	92.7
Co(<i>s</i>)	0.525	H ₂ O(<i>l</i>)	45.9
Au(<i>s</i>)	0.563	Hg(<i>l</i>)	3.91
Pb(<i>s</i>)	2.37	SiCl ₄ (<i>l</i>)	165
Fe(<i>s</i>)	0.56	TiCl ₄ (<i>l</i>)	89
Ge(<i>s</i>)	1.38		

$$\kappa = -\frac{1}{V} \left(\frac{\partial V}{\partial p} \right)_T$$

How are β and κ measured?

One way: measure the density $\rho(T,p)$ of a gas, liquid, or solid at different temperatures and pressures.

$\rho(T,p)$ = mass per unit volume at temperature T , pressure p

Then use:

$$\beta = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_p = -\frac{1}{\rho} \left(\frac{\partial \rho}{\partial T} \right)_p$$

$$\kappa = -\frac{1}{V} \left(\frac{\partial V}{\partial p} \right)_T = \frac{1}{\rho} \left(\frac{\partial \rho}{\partial p} \right)_T$$

- Can you derive the equations for β and κ in terms of the density?
- Are β and κ intensive or extensive quantities?

Exercise: Evaluate the volumetric thermal expansion coefficient for an ideal gas ($V = nRT/p$) at 298 K

$$\begin{aligned}\beta &= \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_p \\ &= \frac{1}{V} \left[\frac{\partial}{\partial T} \left(\frac{nRT}{p} \right) \right]_p \\ &= \frac{1}{V} \left(\frac{nR}{p} \right) \left[\frac{\partial T}{\partial T} \right]_p \\ &= \frac{nR}{pV} = \frac{nR}{nRT} = \frac{1}{T} \\ &= \frac{1}{298 \text{ K}} = 0.00335 \text{ K}^{-1}\end{aligned}$$

ideal gas

$$\beta = \frac{1}{T}$$

Exercise: Evaluate the isothermal compressibility for an ideal gas ($V = nRT/p$) at $p = 1.00$ bar

$$\begin{aligned}\kappa &= -\frac{1}{V} \left(\frac{\partial V}{\partial p} \right)_T \\ &= -\frac{1}{V} \left[\frac{\partial}{\partial p} \left(\frac{nRT}{p} \right) \right]_T \\ &= -\frac{1}{V} (nRT) \left[\frac{\partial p^{-1}}{\partial p} \right]_T \\ &= -\frac{nRT}{V} \left[\frac{-1}{p^2} \right] = \frac{nRT}{pV} \frac{1}{p} = \frac{1}{p} \\ &= \frac{1}{1.00 \text{ bar}} = 1.00 \text{ bar}^{-1}\end{aligned}$$

ideal gas
$\kappa = \frac{1}{p}$

Exercise: For a nonideal gas with second virial coefficient $B(T)$ and the equation of state

$$Z = \frac{pV}{nRT} = 1 + \frac{nB(T)}{V}$$

show that the isothermal compressibility is

$$\kappa = \frac{1}{p + \frac{n^2 RTB(T)}{V^2}} = \frac{1}{p + \frac{RTB(T)}{V_m^2}}$$

Isothermal Compressibility of a Nonideal Gas with Second Virial Coefficient $B(T)$

$$\kappa = \frac{1}{p + \frac{n^2 RTB(T)}{V^2}} = \frac{1}{p + \frac{RTB(T)}{V_m^2}}$$

Significance:

ideal gas with

$$B(T) = 0$$

no molecular interactions

$$\kappa = 1/p$$

nonideal gas with $B(T) < 0$

attractive interactions dominate

$$\kappa > 1/p$$

gas is “more compressible”

nonideal gas with $B(T) > 0$

repulsive interactions dominate

$$\kappa < 1/p$$

gas is “less compressible”

Comparisons:

For an **ideal gas** at 298 K and 1.00 bar:

$$\beta = 0.00335 \text{ K}^{-1}$$

$$\kappa = 1.00 \text{ bar}^{-1}$$

For **liquid water** at 298 K and 1.00 bar:

$$\beta = 0.000204 \text{ K}^{-1}$$

$$\kappa = 0.0000459 \text{ bar}^{-1}$$

For **solid iron** at 298 K and 1.00 bar:

$$\beta = 0.0000369 \text{ K}^{-1}$$

$$\kappa = 0.00000056 \text{ bar}^{-1}$$

-
- the volumes of solids and liquids are much less sensitive to temperature changes than gases
 - solids and liquids are “almost” incompressible ($\kappa \ll 1 \text{ bar}^{-1}$)

Why?

Exercise: 2.00 L of ideal gas at 298 K (25 °C) and 1.00 bar is heated at constant pressure to 323 K (50 °C). Calculate the final volume.

Easy! The equation of state $pV = nRT$ is known. Use:

$$V_f / V_i = (nRT_f / p_f) / (nRT_i / p_i) = T_f / T_i = (323 \text{ K} / 298 \text{ K}) = 1.0839$$

$$V_f = 1.0839 \times 2.00 \text{ L}$$

$$V_f = 2.17 \text{ L}$$

$$\begin{aligned} \% \text{ volume change} &= \frac{V_f - V_i}{V_i} 100\% = \frac{2.17 \text{ L} - 2.00 \text{ L}}{2.00 \text{ L}} 100\% \\ &= 8.5 \% \text{ volume increase} \end{aligned}$$

Exercise: 2.00 L of **liquid** water at 298 K (25 °C) and 1.00 bar is heated at constant pressure to 323 K (50 °C). Calculate the final volume. **Data:** $\beta = 0.000204 \text{ K}^{-1}$ (assumed constant).

Note: The equation of state of liquid water is not provided.

Can't use $pV = nRT$ (liquid H₂O is not an ideal gas). Instead:

$$\beta = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_p \quad \boxed{\times dT_p \Rightarrow} \quad \frac{dV}{V} = \beta dT$$

$$\int_{V_i}^{V_f} \frac{dV}{V} = \int_{T_i}^{T_f} \beta dT \quad \text{Integrate at constant pressure:}$$

$$\ln \left(\frac{V_f}{V_i} \right) = \beta(T_f - T_i) = 0.000204 \text{ K}^{-1} (25 \text{ K}) = 0.0051$$

$$\frac{V_f}{V_i} = e^{0.0051} = 1.0051$$

$$\begin{aligned} V_f &= 1.0051 \times V_i = 1.0051 \times 2.00 \text{ L} \\ V_f &= \mathbf{2.01 \text{ L}} \quad (\text{only a } 0.5 \% \text{ increase}) \end{aligned}$$

Exercise: 2.00 L of ideal gas at 298 K (25 °C) and 1.00 bar is isothermally compressed to a final pressure of 5.00 bar. Calculate the final volume.

Easy! The equation of state $pV = nRT$ is known. Use:

$$V_f / V_i = (nRT_f / p_f) / (nRT_i / p_i) = p_i / p_f = (1.00 \text{ bar} / 5.00 \text{ bar}) = 0.200$$

$$V_f = 0.200V_i = 0.200 \times 2.00 \text{ L}$$

$$V_f = \mathbf{0.400 \text{ L}}$$

$$\begin{aligned} \% \text{ volume change} &= \frac{V_f - V_i}{V_i} 100\% = \frac{0.400 \text{ L} - 2.00 \text{ L}}{2.00 \text{ L}} 100\% \\ &= -80.0 \% \end{aligned}$$

Exercise: 2.00 L of **liquid** water at 298 K (25 °C) and 1.00 bar is isothermally compressed to a final pressure of 5.00 bar. Calculate the final volume. **Data:** $\kappa = 0.0000459 \text{ bar}^{-1}$ (assumed constant).

Note: The equation of state of liquid water is not provided.

Can't use $pV = nRT$ (liquid H₂O is not an ideal gas). Instead:

$$\kappa = -\frac{1}{V} \left(\frac{\partial V}{\partial p} \right)_T \quad \boxed{\times dp_T \Rightarrow} \quad \frac{dV}{V} = -\kappa dp$$

$$\int_{V_i}^{V_f} \frac{dV}{V} = -\int_{p_i}^{p_f} \kappa dp \quad \text{integrate at constant temperature:}$$

$$\ln \left(\frac{V_f}{V_i} \right) = -\kappa(p_f - p_i) = -0.0000459 \text{ bar}^{-1} (4.00 \text{ bar}) = -0.000184$$

$$\frac{V_f}{V_i} = e^{-0.000184} = 0.99982$$

$$\begin{aligned} V_f &= 0.99982 \times V_i = 0.99982 \times 2.00 \text{ L} \\ V_f &= \mathbf{1.99963 \text{ L}} \quad (-0.0184 \% \text{ change}) \\ &\Rightarrow \text{volume almost independent of } p \end{aligned}$$

!!! Warning !!!

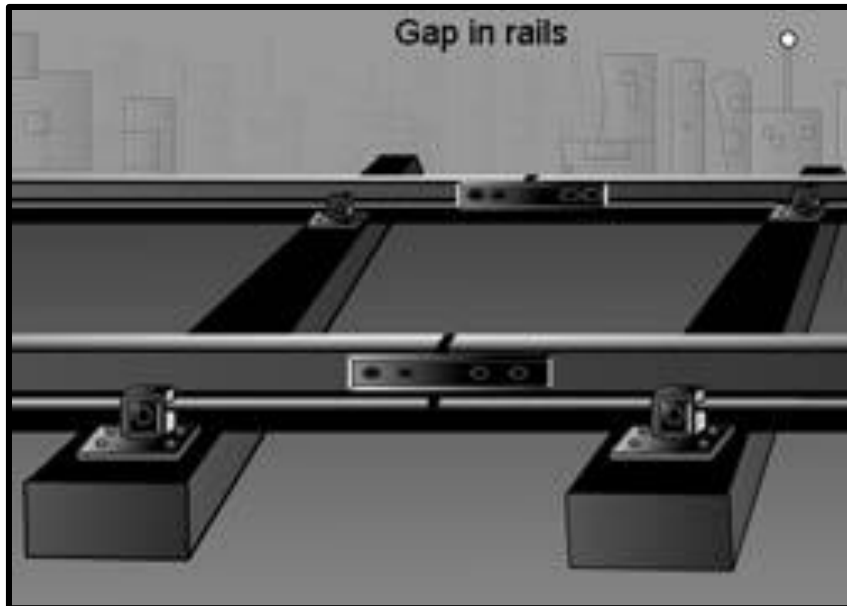
Heating a solid or a liquid at constant volume can produce dangerously large pressure increases.

- Railroads are constructed with small gaps between lengths of steel rails to allow for thermal expansion
- Bridges have small gaps between structural beams
- Liquid-in-glass thermometers break if heated beyond their temperature range
- ***Never fill a container to the brim with a liquid and seal it!***
- Useful application: “shrink fits” used by machinists

What does thermodynamics have to say about $\left(\frac{\partial p}{\partial T}\right)_V$?



Thermal Expansion Gaps





No Thermal Expansion Gaps!

Change in Pressure with Temperature at Constant Volume

$$\left(\frac{\partial p}{\partial T}\right)_V = -\left(\frac{\partial p}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_p$$

Cyclic Rule!

$$= \frac{\left(\frac{\partial V}{\partial T}\right)_p}{-\left(\frac{\partial V}{\partial p}\right)_T}$$

Inverse Rule!

$$= \frac{\frac{1}{V} \left(\frac{\partial V}{\partial T}\right)_p}{-\frac{1}{V} \left(\frac{\partial V}{\partial p}\right)_T}$$

Definition of β , κ

$$= \frac{\beta}{\kappa}$$

ratio of the volumetric thermal expansion coefficient to the isothermal compressibility

Changes in Pressure with Temperature at Constant Volume

For an **ideal gas** at 298 K and 1 bar:

$$\left(\frac{\partial p}{\partial T}\right)_V = \frac{\beta}{\kappa} = \frac{\frac{1}{T}}{\frac{1}{p}} = \frac{p}{T} = \frac{1.00 \text{ bar}}{298 \text{ K}} = 0.00335 \text{ bar K}^{-1}$$

(no problem)

For **solid iron** at 298 K and 1 bar:

$$\left(\frac{\partial p}{\partial T}\right)_V = \frac{\beta}{\kappa} = \frac{0.0000369 \text{ K}^{-1}}{0.00000056 \text{ bar}^{-1}} = 66 \text{ bar K}^{-1}$$

970 lb per square inch per degree !

Uh Oh!

Freezing liquid water in a confined space can split pipes, damage concrete, heave foundations, and crack porous rocks.



Why ?

Exercise: **Liquid water at 0 °C and 1.00 bar is frozen at constant volume. Calculate the final pressure.**

- Data:**
- Ice is less dense than liquid water. (*Ice floats!*) Freezing liquid water produces a 9 % increase in volume.
 - isothermal compressibility of ice $\kappa = 51.0 \times 10^{-6} \text{ bar}^{-1}$

Solution: Freezing water at 1.00 bar increases the volume by 9 %.
To maintain constant volume, the pressure on the ice must be increased to reduce the volume by 9 %.

$$\kappa = -\frac{1}{V} \left(\frac{\partial V}{\partial p} \right)_T \quad \text{multiply by } dp \text{ at constant } T$$

$$\kappa dp = -\frac{dV}{V} \quad \text{integrate from } p_i = 1.00 \text{ bar to } p_f$$

Exercise: **Liquid water at 0 °C and 1.00 bar is frozen at constant volume. Calculate the final pressure.**

$$\int_{p_i}^{p_f} \kappa dp = \kappa \int_{p_i}^{p_f} dp = - \int_{V_i}^{V_f} \frac{dV}{V} \quad \text{assume } \kappa \text{ is constant} \quad (\text{cont.})$$

(no other information given)

$$\kappa(p_f - p_i) = - \ln\left(\frac{V_f}{V_i}\right)$$

$$p_f = p_i - \frac{1}{\kappa} \ln\left(\frac{V_f}{V_i}\right)$$

$$p_f = 1.00 \text{ bar} - \frac{1}{51.0 \times 10^{-6} \text{ bar}^{-1}} \ln\left(\frac{1}{1.09}\right)$$

$$p_f = 1.00 \text{ bar} + 1690 \text{ bar} \approx 1700 \text{ bar}$$

Conclusion: Freezing liquid water at constant volume generates a pressure of about **1700 bar**
($\approx 25,000$ lb per square inch! Uh Oh!)

Sections 3.2 and 3.3 Dependence of the Internal Energy U on Temperature and Volume

- widely used for scientific and engineering calculations
- provides valuable information about molecular energy levels and molecular interactions

Because the internal energy of a system is a state function $U(T,V)$, the differential dU is exact. Mathematics provides:

$$dU = \left(\frac{\partial U}{\partial T} \right)_V dT + \left(\frac{\partial U}{\partial V} \right)_T dV$$

A useful theoretical result. But for practical applications:

How are $(\partial U/\partial T)_V$ and $(\partial U/\partial V)_T$ calculated ?

$$(\partial U/\partial T)_V \quad ???$$

from the First Law: $dU = dq + dw$

only p - V work possible: $dU = dq - p_{\text{external}}dV$

at constant volume: $dU_V = dq_V$
($dV = 0$, no work)

**heat capacity at
constant volume**

$$C_V = \frac{dq_V}{dT} = \left(\frac{\partial U}{\partial T} \right)_V$$

C_V is an experimental quantity, measured using calorimetry.

$$\left(\frac{\partial U}{\partial V}\right)_T \quad ???$$

from Chapters 1 and 2:

$$\left(\frac{\partial U}{\partial V}\right)_T = T \left(\frac{\partial p}{\partial T}\right)_V - p$$

Plan A If the **equation of state of the system is known**, then $(\partial p/\partial T)_V$ and therefore $(\partial U/\partial V)_T$ are easily calculated.

Plan B If the **equation of state of the system is unknown**, then $(\partial p/\partial T)_V$ and $(\partial U/\partial V)_T$ can be calculated using measurable volumetric thermal expansion coefficients (β) and isothermal compressibilities (κ) (see Section 3.1) using

$$\left(\frac{\partial p}{\partial T}\right)_V = \frac{\beta}{\kappa} \qquad \left(\frac{\partial U}{\partial V}\right)_T = T \frac{\beta}{\kappa} - p$$

So What ???

Important result: Changes in the internal energy of any system can be calculated from measurable quantities.

“theoretical”

$$dU = \left(\frac{\partial U}{\partial T} \right)_V dT + \left(\frac{\partial U}{\partial V} \right)_T dV$$

becomes “practical”

$$dU = C_V dT + \left(T \frac{\beta}{\kappa} - p \right) dV$$

in terms of the measurable quantities:

$$C_V = \frac{dq_V}{dT} \quad \beta = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_p \quad \kappa = -\frac{1}{V} \left(\frac{\partial V}{\partial p} \right)_T$$

Exercise: For ideal gases, prove $\left(\frac{\partial U}{\partial V}\right)_T = 0$

Hint: Recall that the volumetric expansion coefficient and isothermal compressibility of an ideal gas are $\alpha = 1/T$ and $\kappa = 1/p$

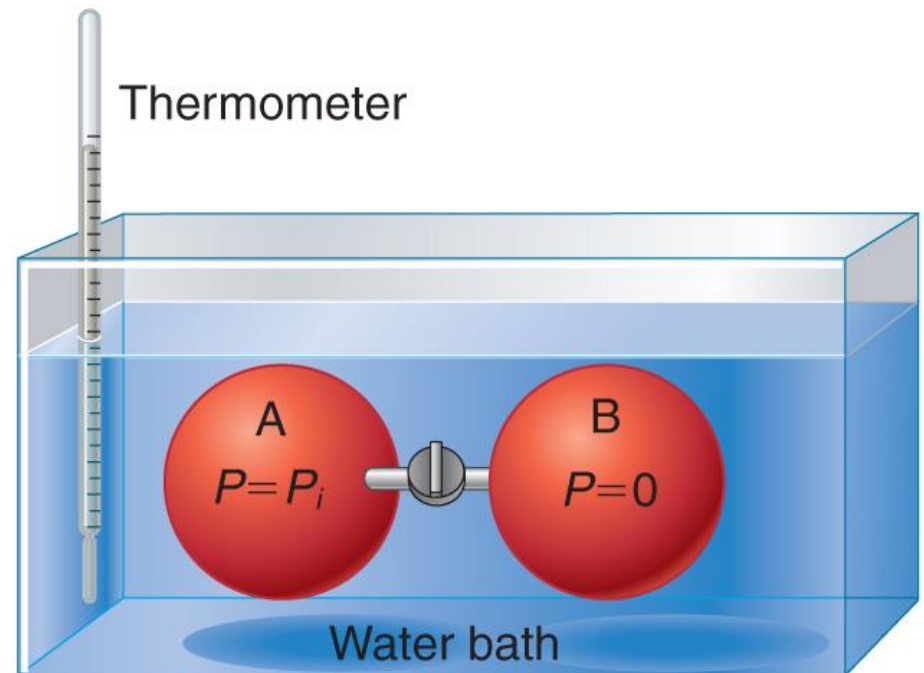
Exercise: Theory is fine, but can you suggest an experiment that could be used to show $(\partial U/\partial V)_T = 0$ for ideal gases?

One possibility:

Open a valve, allow gas at pressure p_i in flask A to expand into evacuated flask B.

If the gas is ideal, what is the change in temperature?

Why?



Sections 3.4 to 3.6 Dependence of the Enthalpy $H = U + pV$ on Temperature and Pressure

- recall from Chapter 2: $q_p = \Delta H$
- as a result, enthalpy changes are important for calorimetry, combustion reactions and other chemical reactions
- also important for flow processes (next Section)

T and p are therefore “natural” variables for the enthalpy.

H is a state function $H(T,p)$, so the **differential dH is exact** and

$$dH = \left(\frac{\partial H}{\partial T} \right)_p dT + \left(\frac{\partial H}{\partial p} \right)_T dp$$

Another useful theoretical result. But for practical applications

how are $(\partial H/\partial T)_p$ and $(\partial H/\partial p)_T$ calculated ?

$$(\partial H/\partial T)_p \quad ?$$

from the First Law: $dU = dq + dw$

only p - V work possible: $dU = dq - p_{\text{external}}dV$

at constant pressure: $dU_p = dq_p - pdV$

$$\begin{aligned}dq_p &= dU_p + pdV = d(U + pV) \\ &= dH\end{aligned}$$

**heat capacity at
constant pressure**

$$C_p = \frac{dq_p}{dT} = \left(\frac{\partial H}{\partial T} \right)_p$$

C_p is an experimental quantity measured using calorimeters operated at constant pressure

$$\boxed{(\partial H/\partial p)_T \quad ?}$$

$$\begin{aligned} dH &= d(U + pV) \\ &= dU + d(pV) \\ &= dU + pdV + Vdp \\ &= (\partial U/\partial T)_V dT + (\partial U/\partial V)_T dV + pdV + Vdp \\ &= C_V dT + [T(\partial p/\partial T)_V - p]dV + pdV + Vdp \end{aligned}$$

$$dH_T = T(\beta/\kappa)dV_T + Vdp_T \quad (\mathbf{dT = 0 \text{ at constant } T, \text{ divide by } dp_T})$$

$$\left(\frac{\partial H}{\partial p}\right)_T = \frac{T\beta}{\kappa} \left(\frac{\partial V}{\partial p}\right)_T + V = \frac{T\beta}{\kappa}(-\kappa V) + V$$

$$\boxed{\left(\frac{\partial H}{\partial p}\right)_T = V(1 - \beta T)} \quad V, \beta, \text{ and } T \text{ are all measurable quantities}$$

So What ???

Important result: Changes in the enthalpy of any system can be calculated from measurable quantities.

“theoretical”
$$dH = \left(\frac{\partial H}{\partial T} \right)_p dT + \left(\frac{\partial H}{\partial p} \right)_T dp$$

becomes “practical”

$$dH = C_p dT + V(1 - \beta T) dp$$

in terms of the measurable quantities:

$$C_p = \frac{dq_p}{dT} \quad \beta = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_p$$

Exercise: **For ideal gases, show**

$$\left(\frac{\partial H}{\partial p} \right)_T = 0$$

As a result, the enthalpy of an ideal gas depends only on temperature and

$$dH = C_p dT \quad (\text{even if } p \text{ is changing!})$$

Exercise: **For liquids and solids, show**

$$\left(\frac{\partial H}{\partial p} \right)_T \approx V$$

As a result

$$dH \approx C_p dT + V dp \quad (\text{liquids and solids})$$

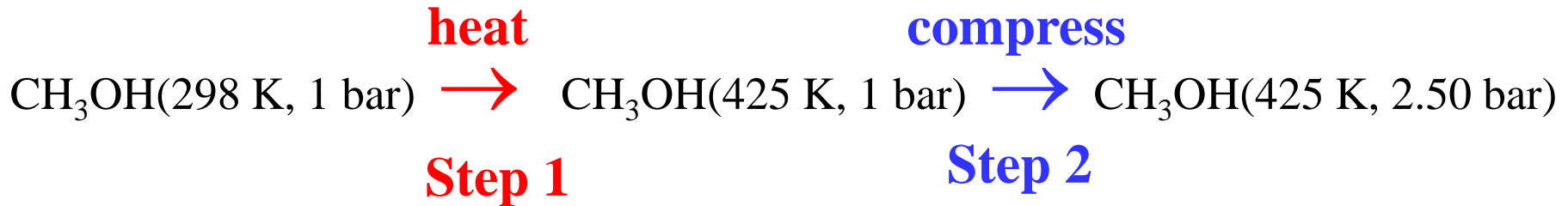
Example Problem 3.9

Calculate the change in enthalpy when 124 g of liquid methanol at 1.00 bar and 298 K is heated and compressed to 2.50 bar and 425 K .

Data: methanol molar mass	$M = 32.04 \text{ g mol}^{-1}$
density of liquid methanol	$\rho = 0.791 \text{ g cm}^{-3}$
heat capacity of liquid methanol	$C_{pm} = 81.1 \text{ J K}^{-1} \text{ mol}^{-1}$

Solution:

Enthalpy is a state function, so ΔH can be calculated for any path between the initial and final states. We will heat first, then compress:



Example Problem 3.9 (cont.)

Step 1 Heat 124 g of liquid methanol from 289 K to 425 K at 1 bar.

$$\Delta H_p = \int_{T_i}^{T_f} C_p dT = nC_{pm} \int_{T_i}^{T_f} dT = nC_{pm}(T_f - T_i)$$

$$\Delta H_p = \frac{124 \text{ g}}{32.04 \text{ g mol}^{-1}} (81.1 \text{ J K}^{-1} \text{ mol}^{-1}) (425 \text{ K} - 298 \text{ K}) = 39,900 \text{ J}$$

Step 2 Compress 124 g of liquid methanol from 1.00 bar to 2.50 bar at a constant temperature of 425 K.

$$\Delta H_T = \int_{p_i}^{p_f} \left(\frac{\partial H}{\partial p} \right)_T dp \approx \int_{p_i}^{p_f} V dp \approx V \int_{p_i}^{p_f} dp = V(p_f - p_i)$$

$$\Delta H_T = (124 \text{ g} / 0.791 \text{ g cm}^{-3})(10^{-6} \text{ m}^3 \text{ cm}^{-3})(2.50 - 1.00 \text{ bar})(10^5 \text{ Pa bar}^{-1}) = 39.9 \text{ J}$$

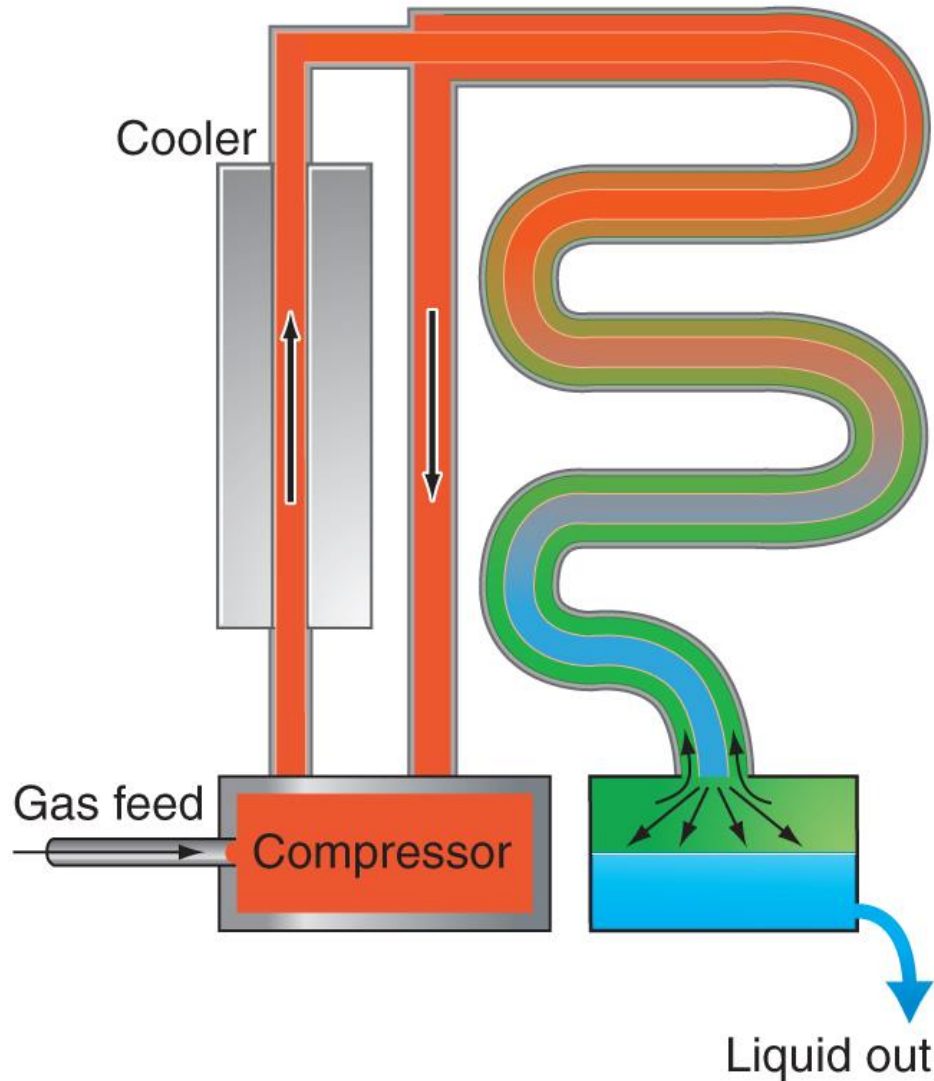
$$\begin{aligned} \text{Overall } \Delta H &= \Delta H_p \text{ (step 1)} + \Delta H_T \text{ (step 2)} \\ &= 39,900 \text{ J} + 40 \text{ J} \\ &\approx 39,900 \text{ J from step 1} \end{aligned}$$

For solids and liquids, changes in pressure usually cause small enthalpy changes

Section 3.7 The Joule-Thomson (JT) Experiment

- irreversible expansion of gas through a porous barrier or throttle valve under adiabatic conditions (no heat flow)
- ideal gases: no temperature change
- real gases: can **cool down** or **warm up** during JT expansion
- important applications
 - * refrigeration
 - * air conditioning
 - * heat pumps
 - * gas liquefaction

Gas Liquefaction



For **industrial applications**:

(not university lab experiments!)

- **continuous flow** (more economical than batch processing)
- **re-cycle** gas that does not liquefy (no wastage)
- **heat-exchange** – use cool gas that does not liquefy to pre-cool gas from compressor
- **large-scale production** (thousands of tons per day)
- use the expanding gas to **run a generator** (adiabatic cooling)

Applications of Liquefied Gases

- **liquid air** is distilled to produce liquid N_2 and liquid O_2
- N_2 is used to make **ammonia** for the production of nitric acid, fertilizers, explosives, and many other industrial chemicals
- cold liquefied natural gas (**LNG**) can be shipped economically over large distances in **cheap low-pressure tanks** (at ≈ 1 atm)
- liquid N_2 and liquid He are important **cryogen**s
(liquid He is used to operate superconducting nmr magnets)
- **liquid propane** allows barbecuing without charcoal
- many other important uses

Refrigeration and Air Conditioning

- expanding nonideal gases cool and absorb heat
- keeps perishable food products fresh, nutritious and safe to eat
- air conditioners provide cooling and humidity reduction, making large regions “habitable” for “modern” people

**Ever tried working (or living)
at 30 °C and 95 % humidity?**



LNG Ship Carrying Liquefied Natural Gas (at about $-260\text{ }^{\circ}\text{C}$)



Application of Liquefied Gases: Space Exploration

store liquid fuel and oxidizer in
light thin-wall low pressure tanks

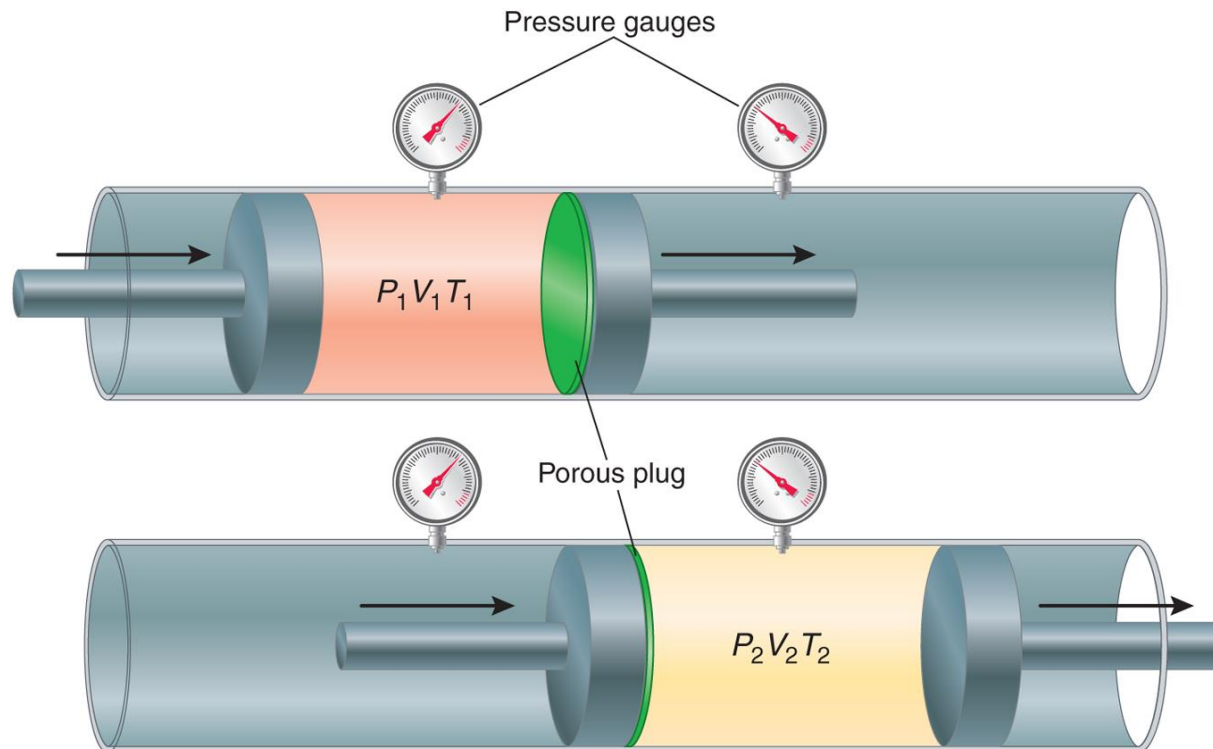
Saturn V Heavy-Lift Vehicle ("Apollo Moon Rocket")

- most powerful rocket ever built
- operational 1967 to 1973
- 7.6 million pounds thrust
- launched 130-ton payloads into earth orbit
- never failed, even when hit by lightning (Apollo 12 mission)
- kerosene / **liquid oxygen** first stage
- **liquid hydrogen** / **liquid oxygen** second and third stages
- mileage: about five inches per gallon



Joule Thomson (JT) Flow Experiment – *How does it work?*

- gas initially at p_1, V_1, T_1
- expands **adiabatically** through a porous plug or throttle valve
- gas downstream leaves at p_2, V_2, T_2



work $p_1 V_1$ done
on the gas to force
it through the plug

work $p_2 V_2$ done
on the surroundings
by the expanding gas

Thermodynamic Analysis of Joule-Thomson (JT) Expansions

$$p_1, V_1, T_1 \rightarrow p_2, V_2, T_2$$

$$\text{First Law: } \Delta U = \cancel{q} + w$$

$$U_2 - U_1 = p_1V_1 - p_2V_2$$

$$U_2 + p_2V_2 = U_1 + p_1V_1$$

$$H_2 = H_1$$

$$\Delta H = 0$$

Conclusion: Joule-Thomson expansions are “**isenthalpic**”
(occur at constant enthalpy)

Joule-Thomson Coefficient of Performance

$$\mu_{\text{JT}} = \left(\frac{\partial T}{\partial p} \right)_H$$

μ_{JT} gives the change in temperature per unit change in pressure of the expanding gas. But what is μ_{JT} ?

Using the **cyclic and inverse rules** of partial derivatives:

$$\mu_{\text{JT}} = \left(\frac{\partial T}{\partial p} \right)_H = - \left(\frac{\partial T}{\partial H} \right)_p \left(\frac{\partial H}{\partial p} \right)_T = - \left(\frac{\partial H}{\partial p} \right)_T / \left(\frac{\partial H}{\partial T} \right)_p$$

$$\mu_{\text{JT}} = - \frac{V(1 - \beta T)}{C_p}$$

Gives temperature change of the expanding gas in terms of **measurable quantities**.

TABLE 3.3 Joule-Thomson Coefficients for Selected Substances at 273 K and 1 atm

Gas	μ_{J-T} (K/MPa)
Ar	3.66
C ₆ H ₁₄	-0.39
CH ₄	4.38
CO ₂	10.9
H ₂	-0.34
He	-0.62
N ₂	2.15
Ne	-0.30
NH ₃	28.2
O ₂	2.69

$$\mu_{JT} = \left(\frac{\partial T}{\partial p} \right)_H$$

$\mu_{JT} > 0$: expanding gas cools down
 $\Delta T < 0$ if $\Delta p < 0$

$\mu_{JT} < 0$: expanding gas warms up
 $\Delta T > 0$ if $\Delta p < 0$

Which of the listed substances would make the best refrigerant? *Why?*

Exercise: Evaluate the Joule-Thomson coefficient μ_{JT} for an ideal gases.

$$\mu_{\text{JT}} = -\frac{V(1 - \beta T)}{C_p}$$

For an ideal gas ($pV = nRT$), recall $\beta = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_p = \frac{1}{T}$

which gives $\mu_{\text{JT}} = -\frac{V(1 - \frac{1}{T}T)}{C_p} = 0$ **(ideal gas)**

Conclusion: Warming or cooling during Joule-Thomson expansions occurs only for nonideal gases (molecular interactions).

Why Does **Warming** or **Cooling** Occur During JT Expansions?

For a nonideal gas obeying the van der Waals equation with attractive a and repulsive b coefficients

$$p = \frac{nRT}{V - nb} - \frac{n^2 a}{V^2}$$

the Joule-Thomson coefficient is

$$\mu_{JT} = \frac{1}{C_{pm}} \left(\frac{2a}{RT} - b \right)$$

Joule-Thomson Coefficient of a Nonideal van der Waals Gas

$$\mu_{JT} = \left(\frac{\partial T}{\partial p} \right)_H = \frac{1}{C_{pm}} \left(\frac{2a}{RT} - b \right)$$

Low Temperatures:

$$(2a/RT) - b > 0$$

$$\mu_{JT} > 0$$

Cooling on Expansion. Attractive forces dominate.

“Sticky” molecules fly apart more slowly, with less kinetic energy.

High Temperatures:

$$(2a/RT) - b < 0$$

$$\mu_{JT} < 0$$

Warming on Expansion. Repulsive forces dominate.

Repelling molecules fly apart more quickly, with more kinetic energy.

Max. Inversion temperature: $(2a/RT) - b = 0$

$$\mu_{JT} = 0$$

No temperature change. Attractive and repulsive forces balanced at the Boyle (not Boil!) temperature $T_{\text{Boyle}} = 2a/Rb$.

Isenthalps: States of Constant Enthalpy

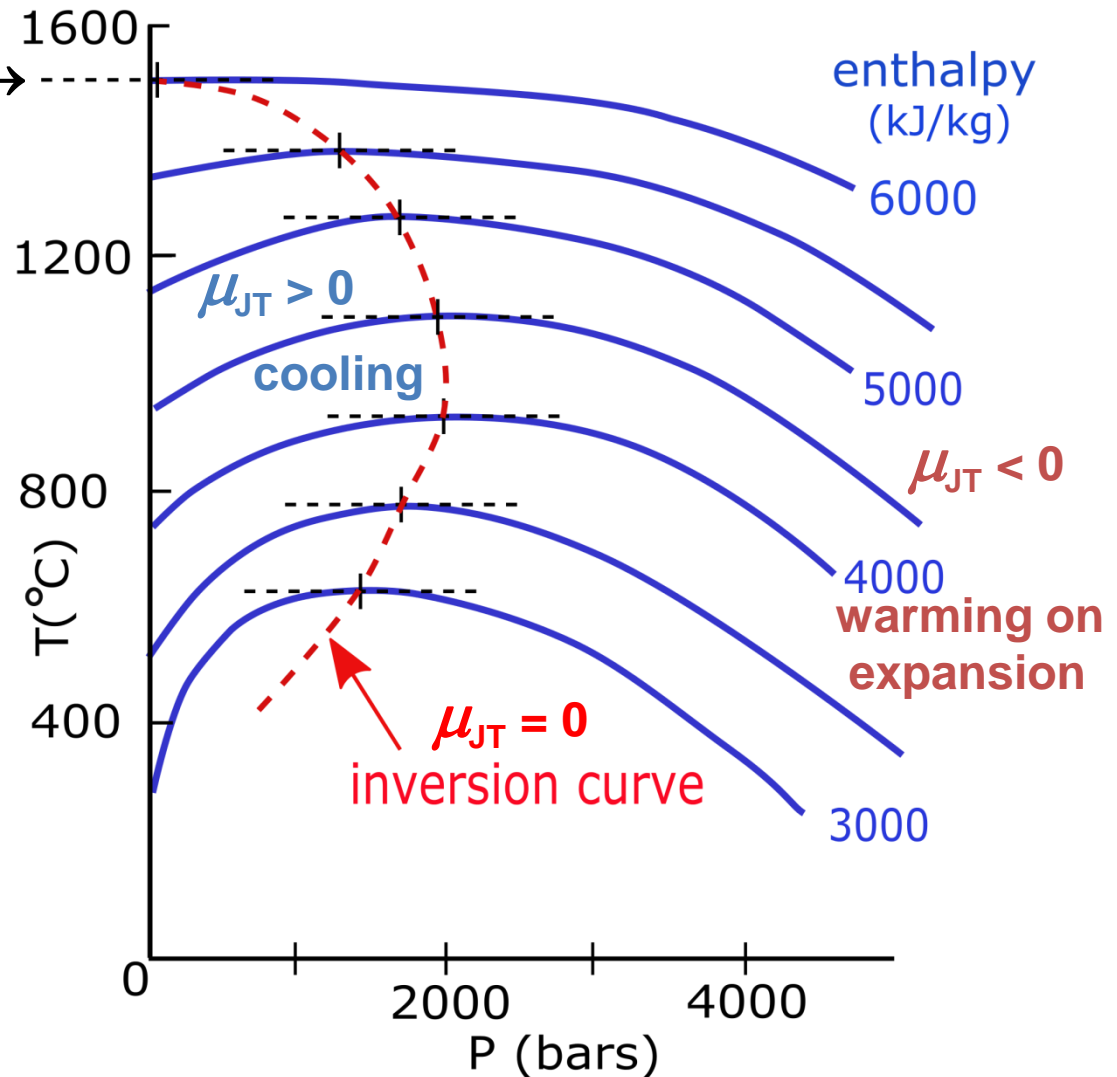
Boyle temperature
(max. inversion temp.)

Graphical interpretation
of the Joule-Thomson
coefficient:

isenthalp slope:

$$\left(\frac{\partial T}{\partial p} \right)_H = \mu_{JT}$$

(JT coefficient)



Joule-Thomson Inversion Temperatures for N₂ and H₂

Use liquid N₂ to cool liquid H₂ below its inversion temperature.

Then use liquid H₂ to cool and liquefy He.

Liquid helium is the ultimate cryogen.

Used for super-conducting magnets and low-temperature research ($T < 4 \text{ K}$).

